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Study of an adaptive optics for the astronomy in the visible

WFS study part

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Part I

Optimization of an adaptive optic system

Chapter I.1

Study of an wavefront sensor: The Shack-Hartmann

I.1.1 Introduction

In this chapter, I present a study of the Shack-Hartmann wavefront sensor (SH). The goal is to optimize the slopes measurement in the SH, thus the wavefront deformation, to get better performance of a given adaptive optics (AO). The main conclusion of this study is that there is no miracle solution for all AO, but the best algorithm depends on the AO considered.

Three main problem are highlighted in this study:

- Detectability at low flux. In a "classical" AO using a natural guide star, the number of photons on the CCD is low. Therefore, even with low readout noise, there is a problem of signal detectability against the noise and trustability of the measurements;
- Noise propagation in presence of medium flux;
- Saturation and/or linearity problem at high flux especially in open loop.

In this part, I first describe the context and the different centroid algorithms such as the center of gravity (CoG), the windowing and thresholding, the weighted center of gravity (WCoG) and correlation. In a second part, I present the optimization of those methods, first without any atmospheric turbulence (Gaussian or diffraction limiter spot) and then with atmospheric turbulence. In addition, the paper describes two special cases: the Planet Finder and the SOAR AO, SAM.

In this report, I will only consider one square sub-aperture. Its dimensions are $d \times d$ (m). The region of interest on the CCD is $W_{fov} \times W_{fov}$ (λ/d).

I.1.2 Problem description

It is necessary to precisely measure the spot position on a SH. Table I.1.1 gathers all the parameters and notations used in the study.

Table I.1.1: List of parameters and notations

Notation	Parameter	Value	Unit
N_{ph}	Number of photons per subaperture and frame	[30, 10000]	photons
N_r	Readout noise per pixel and frame	[0, 3]	électrons
SNR	Signal to noise ratio = N_{ph}/N_r		
$I(x, y)$	Image intensity at the pixel (x, y)		photons
$N_{tot} \times N_{tot}$	Dimension of the calculation window	<32×32	pixels
Dep_{amp}	Spot motion amplitude rms	0.1	pixels
N_T	FWHM of the image spot	[1-2]	pixels
σ	Spot size rms		pixels
	$\frac{N_{samp}}{2\sqrt{2\ln(2)}}$ for a Gaussian spot	0.85	pixels
N_{samp}	FWHM of the diffracted spot	[1-2]	pixels
p	Pixel size(= λ/d)/ N_{samp})		rad
$d \times d$	Subaperture size	0.4	meter
λ	Wavelength		microns
$W_{fov} \times W_{fov}$	Subaperture field of view	<16×16	λ/d
r_0	Fried diameter	[$d/5, 2 * d$]	meter
T	Percentage of the maximum defining the threshold value in the thresholding method	0.2	
$W \times W$	Region of calculation in the windowing method	[4-32]	pixels
$P(x, y)$	Reference function, Gaussian		
$I_c(x, y)$	Correlation function		photons ²
n	"Oversampling" factor of the correlation	[1-4]	
$N_c \times N_c$	Size window for the correlation	$n^*[16-64]$	pixels
$W_c \times W_c$	region of calculation of the correlation peak	[3-32]	pixels
N_w	FWHM of the reference function		pixels
K_s	Factor defining N_w such as $N_w = K_s N_{samp}$	[1-16]	
δ	FWHM of the I_c		pixels
T_{corr}	Percentage of the maximum defining the threshold value for I_c peak determination by CoG		
$\sigma_{\Delta\phi}^2$	Phase error variance		radians ²
D_x, D_y	Know center of mass	[-0.5, 0.5]	pixels
$(C_{mes})_x, (C_{mes})_y$	Measured center of mass		pixels
α	Response coefficient		

Comments:

- The window size is expressed either in pixels or in λ/d , where λ/d is the size of the diffraction spot produced by the subaperture. Three spot shapes have been studied: Gaussian spot, diffraction spot, diffraction spot distorted by the turbulence. For all three cases, the pixel size and the FoV size are relative to λ/d .

- Signal to noise ratio definition (SNR): the SNR can have several definitions. In this report, I use SNR for $SNR = N_{ph}/N_r$, where N_{ph} is the mean number of photons per subaperture and frame and N_r the readout noise per pixel and frame.

I.1.2.1 Noise

The noise term gathers readout noise, photon noise, and noise due to the atmospheric turbulence. Fig. I.1.1, I.1.2, I.1.3 show the images obtained at the focal plane of a square lenslet in the case of a perfect wavefront – figure I.1.1 –, for a wavefront distorted by atmospheric turbulence – figure I.1.2 –, and finally for a wavefront distorted by atmospheric turbulence in presence of readout noise and photon noise – figure I.1.3. All the spot are Nyquist sampled.

From those images, it is obvious that the centroid calculation will be affected by those different noise. The goal is to find a algorithm that *minimizes the noise propagation, linear and robust*.

- **Good noise propagation:** to minimize the noise impact on the CoG calculation. We will adjust the parameters (T , W , T_{corr} ...) to decrease the noise variance. It is important to note that this is not the propagation noise in the OA system but only the noise propagation to the spot position determination;
- **Linearity and response coefficient:** we want to get an unbiased measure meaning that for a spot motion D_x , I measure the same motion D_x and not αD_x where $\alpha < 1$. Moreover, we want to get a linear response. Therefore, if the measured spot position is written $(C_{mes})_x = \alpha D_x + \beta$, where β is the non-linearity coefficient, we want $alpha = 1$ and $\beta = 0$.
- **Robustness** when the SNR is low, the reliability of the measurement is low. One way to overcome this limitation is to disregard the measures that are a priori false. (cf section I.1.4.2).

I.1.2.2 Merit function

The parameter to evaluate the performance is the error variance σ_{err} , calculated from the error made on the spot position estimation. σ_{err} is in *pixels*²:

$$\sigma_{err}^2 = \langle (C_{mes} - D_x)^2 \rangle, \quad (I.1.1)$$

where D_x is the true value of the center of mass, C_{mes} is the measured value of the center of mass and $\langle . \rangle$ is the classical mean.

The parameters varying in this study are:

- the number of photons or the SNR (c.f. section I.1.2) in presence of readout noise;
- d/r_0 to quantify the amount of atmospheric turbulence;
- the parameters of each algorithm: T and T_{corr} , N_w .

The general expression of the position estimator is

$$C_{mes} = \alpha D_x + f_{nl}(D_x) + \epsilon + noise, \quad (I.1.2)$$

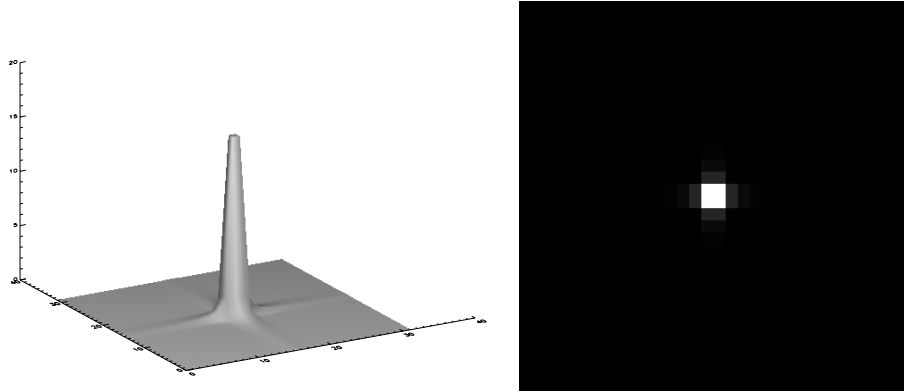


Figure I.1.1: diffraction spot at the lenslet focal plane. The subaperture is square with a FoV of $16 \times 16 \lambda/d$. The wavefront is perfect and there is no noise.

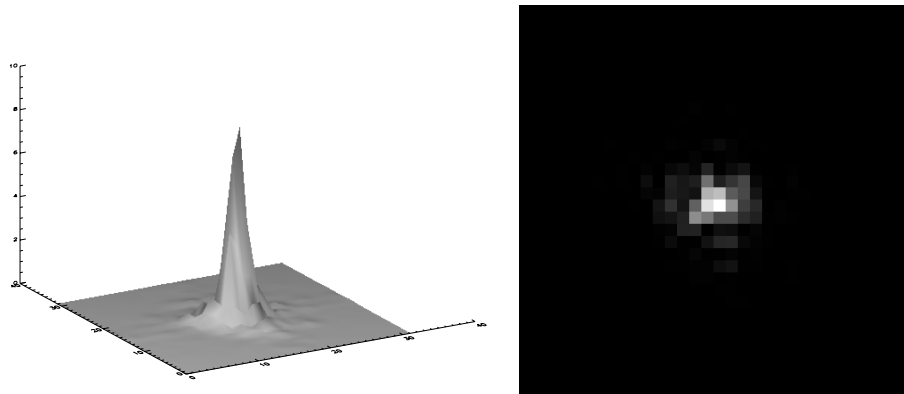


Figure I.1.2: Image spot at the focal of a lenslet, in presence of atmospheric turbulence, $d/r_0 = 2$. The subaperture is square with a FoV of $16 \times 16 \lambda/d$. There is no noise.

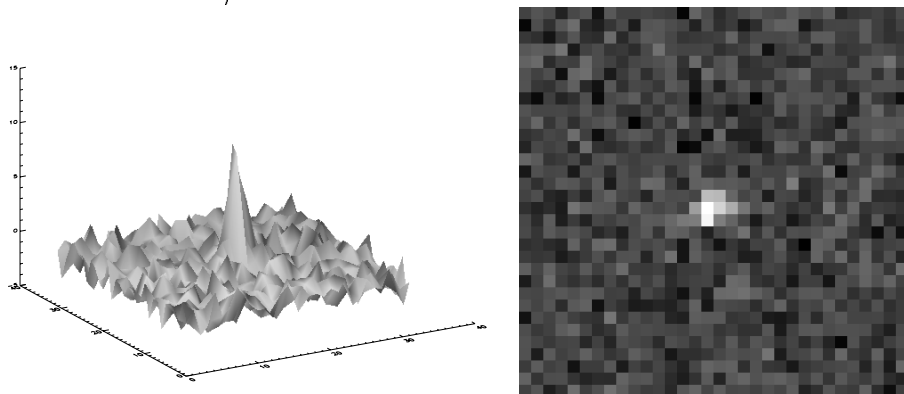


Figure I.1.3: Image spot at the focal of a lenslet, in presence of atmospheric turbulence, $d/r_0 = 2$, readout noise ($N_r = 1$) and photon noise. The subaperture is square with a FoV of $16 \times 16 \lambda/d$ and the flux per subaperture and frame is 100 photons.

where α is the response coefficient, f_{nl} the non-linearity function of the considered algorithm and ϵ the errors due to the spot shape. The term *noise* corresponds to photon noise and readout noise. We then write:

$$\sigma_{\Delta\Phi}^2 = \langle [(\alpha - 1)D_x + f_{nl}(D_x) + \epsilon + \text{bruit}]^2 \rangle \quad (\text{I.1.3})$$

$f_{nl}(x)$ can be defined by the Taylor derivation around D_x . The constant and the linear terms are by definition null. Moreover, we assume that $f_{nl}(x)$ is symmetric against $x = D_x$, leading to a null quadratic term. Thus we can approach it by:

$$f_{nl}(D_x) \approx \beta D_x^3, \quad (\text{I.1.4})$$

where β is the cubic coefficient.

It is logical to assume that the photon noise and the readout noise are not correlated to the spot shape and position. Also we have $\sigma_{noise}^2 = \langle [noise]^2 \rangle$ equal to the sum of two terms $\sigma_{\Delta\Phi, N_r}^2$ and $\sigma_{\Delta\Phi, N_{ph}}^2$. Other less obvious assumptions are made: 1) ϵ and D_x are not correlated and 2) α is constant (which is true for Gaussian spots or if there is no atmospherical turbulence i.e. $d/r_0 < 1$). Finally, the response coefficient α has been adjusted to 1. Equation I.1.3 then becomes:

$$\sigma_x^2 = \sigma_{\Delta\Phi, N_r}^2 + \sigma_{\Delta\Phi, N_{ph}}^2 + \beta^2 \langle D_x^6 \rangle + \langle \epsilon^2 \rangle. \quad (\text{I.1.5})$$

I.1.2.3 Link between simulation and theory

The final *parameter* is the error variance (σ_{err})² given in *pixels*². Most of the graphs in this report show the phase error variance ($\sigma_{\Delta\phi}$)² in radians² versus the photon noise. The link between the two variances is:

$$\sigma_{\Delta\phi}^2 = \sigma_{err}^2 * (2\pi/N_{samp})^2. \quad (\text{I.1.6})$$

This relationship results from the definition of the phase difference ϕ for a motion of one pixel at the lenslet array:

$$\phi = \frac{2\pi}{\lambda} * \delta_{opd}, \quad (\text{I.1.7})$$

where δ_{opd} is the optical difference (OPD) $\delta_{opd} = \alpha_{pix}d$, where α_{pix} is the incoming angle shown on Fig. I.1.4. For a sampling of the diffraction spot equal to N_{samp} , $\alpha_{pix} = (\lambda/d)/N_{samp}$. Therefore, 1 pixel on the detector correspond to a phase difference of ϕ :

$$\phi = \frac{2\pi}{\lambda} \frac{\lambda}{d} \frac{1}{N_{samp}} d = \frac{2\pi}{N_{samp}} \quad (\text{I.1.8})$$

We give in this report the error variance of the phase ϕ . Often in the literature, one gives the error variance of the incoming angle (α) either in CCD pixels or in arcsec. Those two parameters are linked by:

$$\sigma_{err}^2 = \sigma_{\Delta\phi}^2 * \left(\frac{N_{samp}}{2\pi} \right)^2 \text{ pixels}^2, \quad \sigma_{\alpha}^2 = \sigma_{\Delta\phi}^2 * \left(\frac{\lambda/d}{2\pi} \right)^2 \text{ rad}^2 \quad (\text{I.1.9})$$

For example, if $N_{samp} = N_T = 2.355\sigma$, $\sigma_{err}^2 = 1$ pixel corresponds to $\sigma_{\Delta\phi} = 2\pi/2.355 = 2.67$ rad, and therefore to a phase error variance of 7.1 rad².

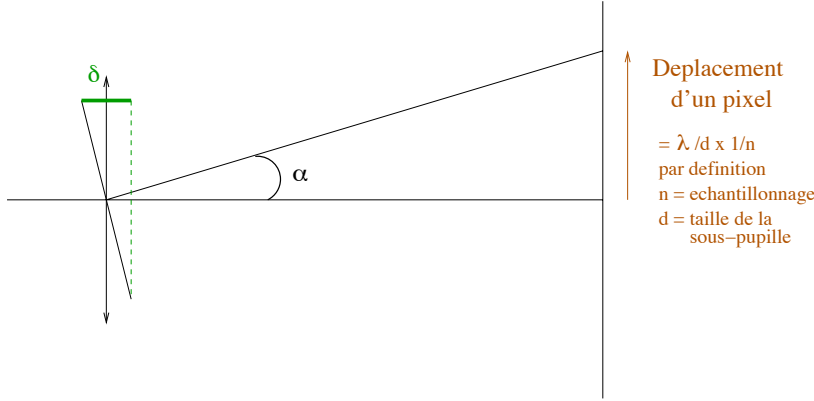


Figure I.1.4: Relationship between the spot motion in pixels and the slope of the wavefront in radians.

I.1.3 Algorithms

I.1.3.1 "Direct" methods

"Direct" methods are the ones used to directly process the image itself. I will consider here the center of gravity (CoG), the thresholding, the windowing, the weighted center of gravity (WCoG) and the quad cell (QC). The goal is to consider in the measurement only pixels with signal. The problem comes from the fact that usually those methods depend on the detection of the maximum position and thus are not reliable a low flux. For the windowing and the WCoG, one solution is to keep the window fixed introducing however some truncation noise.

The simple CoG

The CoG is the intrinsic way to calculate the position of a spot. Given an image of size $N \times N$ corresponding to a subaperture, with the intensity repartition $I_{x,y}$, the center of mass $(C_{mes})_x$, is:

$$(C_{mes})_x = \frac{\sum_{x=-N/2}^{N/2} \sum_{y=-N/2}^{N/2} I_{x,y} \times x}{\sum_{x=-N/2}^{N/2} \sum_{y=-N/2}^{N/2} I_{x,y}}, \quad (\text{I.1.10})$$

This approach is at the same time very precise (especially for high SNR) and easy to implement, explaining why it is broadly used in AO. However, this method is not optimal because of the amplification of the noise for the pixels on the edge.

Analytical expression.

The analytical expression of the error variance in presence of readout noise and photon noise have been introduced by G. Rousset [Rousset, 1999]. The readout noise is a Gaussian noise centered and uniform while the photon noise is poissonian. The formula have been derived in the case of a Gaussian and Nyquist sampled spot.

$$\sigma_{\Delta\phi, N_r}^2 = \frac{\pi^2 N_r^2 N_s^4}{3 N_{ph}^2 N_{samp}^2} \text{ radians}^2 \text{ readout noise} \quad (\text{I.1.11})$$

$$\sigma_{\Delta\phi, N_{ph}}^2 = \frac{\pi^2}{2 \ln 2} \frac{1}{N_{ph}} \left(\frac{N_T}{N_{samp}} \right)^2 \text{ radians}^2 \text{ photon noise.} \quad (\text{I.1.12})$$

where N_T is the FWHM of the image spot in pixels, N_s^2 is the total number of pixels used in the calculation and $N_{samp} = (\lambda/d)/p$, where p is the pixel size in *rad*. I used this definition for N_{samp} even for a Gaussian spot since this function is a first approximation of the diffraction spot. By

definition, I consider a Gaussian function of FWHM equal to $N_{samp} = \lambda/d$. This approximation is in some cases too brutal and it will be better to consider directly the diffraction limited spot, for which the intensity repartition is a $sinc^2$ function. However, the formula I.1.11 are not always valid. In both cases, $N_T = N_{samp}$.

In theory, the CoG method is linear with a response coefficient equal to 1. In practice, the detectors are of finite sizes, which leads to a bias as well as possible non-linearity. For a Gaussian spot of rms size σ and centered on $(D_x, 0)$, the expression of the center of mass, $(C_{mes})_x$ calculated over a window W is [Fusco et Nicolle, 2005]:

$$(C_{mes})_x = D_x - \sigma \sqrt{\frac{2}{\pi}} \frac{e^{-A^2} - e^{-B^2}}{\Phi(B) + \Phi(A)}, \quad (\text{I.1.13})$$

where $\Phi(t) = \frac{2}{\sqrt{\pi}} \int_0^t e^{-u^2} du$, $A = \frac{W/2 - D_x}{\sigma\sqrt{2}}$ et $B = \frac{W/2 + D_x}{\sigma\sqrt{2}}$

The comparison between simulation and theory (Eq. I.1.13) is very good.

Moreover, if $W/2 > 2\sqrt{2}\sigma$, true only if D_x is small ($D_x \ll 1$), then:

$$C_x \simeq D_x - \sigma_{spot} \sqrt{\frac{2}{\pi}} e^{-\frac{(W/2)^2}{2\sigma_{spot}^2}} \left[\frac{W D_x}{\sqrt{2}\sigma_{spot}} + \frac{1}{6} \left(\frac{W D_x}{\sqrt{2}\sigma_{spot}} \right)^3 \right] \quad (\text{I.1.14})$$

This equation can be written as the sum of two terms: the response coefficient and the non-linearity coefficient:

$$(C_{mes})_x \simeq \underbrace{\left(1 - \sigma \sqrt{\frac{2}{\pi}} e^{-\frac{(W/2)^2}{2\sigma^2}} \right)}_{\alpha} \underbrace{\left(\frac{W}{\sqrt{2}\sigma} \right)}_{\beta} D_x - \frac{1}{6} \underbrace{\left(\frac{W}{\sqrt{2}\sigma} \right)^3}_{\beta} D_x^3 \quad (\text{I.1.15})$$

Note that α is close to 1. The deviation from 1 is less than 2.5 % for a $2\lambda/D$ window size and is less than 0.04 % for a $3\lambda/D$ window size.

Windowing

This method consists in reducing the size of interest region on the detector before applying the CoG, disregarding the pixels on the edges that do not a priori have information on the signal.

There are two ways of using the windowing: with a fixed window or a mobil window. For the fixed window, the region is a square box of size $W \times W$ pixels centered on the FoV. For a mobil window, the region is a circular box of diameter W centered on the pixel of maximum intensity (D_x, D_y) (c.f. I.1.5). In both cases, the pixels located outside the box are set to zero. There is a significative difference between the two methods: the window is not centered on the same place: for the fixed window, the center is the center of the subaperture, at the intersection of 4 pixels while for a mobil window the center is a pixel (c.f. Fig I.1.5).

In the case of a mobil window one needs to know the approximate position of the spot which is harder to get when the SNR is low.

Thresholding

For this method, the threshold is first calculated by either taking a percentage T of the maximum when the SNR is high enough or by using the readout noise – for example 2^*N_r – for low SNR.

Window Definition

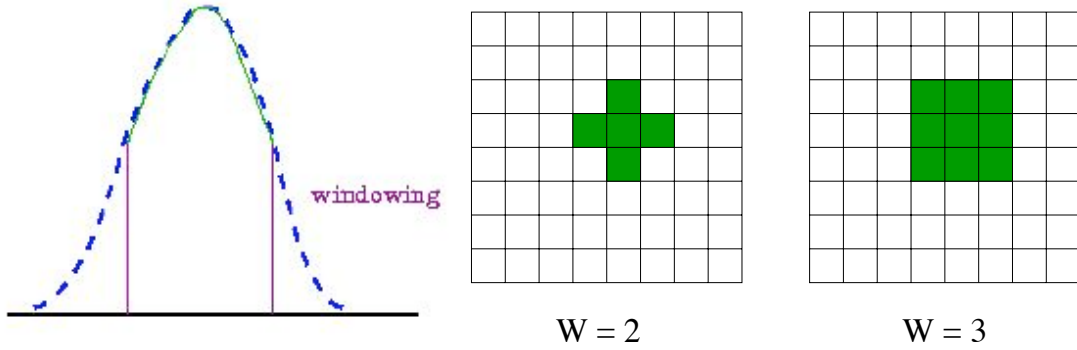


Figure I.1.5: Windowing. The two graphs describe the choice of the pixels in the case of a mobil window.

Once the threshold defined, there are two ways to actually threshold, as shown on Fig. I.1.6. In the first method, (c.f. Fig. I.1.6-I), the threshold is subtracted to the image and the pixels with negative intensity values are set to zero before using the CoG. In the second method (c.f. Fig I.1.6-II), the threshold is not subtracted, the pixels with intensity values less than the threshold are set to zero.

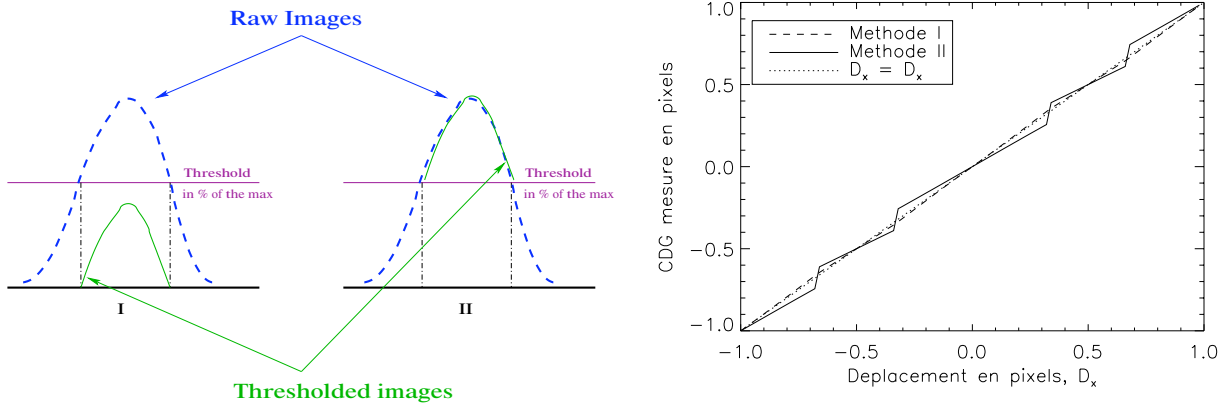


Figure I.1.6: Thresholding. On the left: illustration of the two thresholding methods I and II. $T = 0.1$. On the right: linearity of the two methods. In the simulation we will use method I.

The thresholding I is more reliable since linear. Indeed, let $I(x, y)$ be the intensity at the pixel (x, y) and $I'(x, y)$ the thresholded intensity such as $I'(x, y) = I(x, y) - s$, where s is the threshold value. The center of mass calculated on the domain N^2 of the non null pixels is for both cases I and II:

$$\begin{cases} I : [(C_{mes})_I] = \frac{\sum I'(x, y)x}{\sum I'(x, y)} \\ II : [(C_{mes})_{II}] = \frac{\sum I(x, y)x}{\sum I(x, y)} = \frac{\sum (I'(x, y)x + sx)}{\sum I'(x, y) + s} = \frac{\sum I'(x, y)x}{\sum I'(x, y) + N_s^2 * s} \end{cases} \quad (I.1.16)$$

Fig I.1.6-right shows the center of mass measured versus the true position of the spot for thresholding I and II. It is obvious that the method II introduces a bias, which is confirmed by eqs. I.1.16. The bias α is equal to:

$$\alpha = \left[1 + \frac{N_s^2 * s}{\sum I'(x, y)} \right]^{-1}. \quad (I.1.17)$$

Comments on the windowing and thresholding.

The thresholding and the windowing in the case of a mobil window depend on the direct detection of the maximum and are therefore very sensitive to noise and not very reliable at low SNR. But they are fast, easy to implement, and reliable for a medium SNR (such as a readout noise of 3 per pixel and a number of photon equal to 100 per subaperture).

The quad cell (QC)

The QC is a particular case of windowing where the size of the window is 2×2 pixels, in order to reduce the number of pixel to the minimum needed. There is a difference in the center of mass calculation, which will have its importance in the following:

$$(C_{mes})_x = \gamma \frac{\sum_i I(0 : N/2 - 1, i) - \sum I(N/2 : N - 1, i)}{\sum I} \quad (\text{I.1.18})$$

where γ is in pixels and is related to the response coefficient.

The QC has different advantages: it is fast computationally and it reduced the noise propagation, which explain its use in astronomy because it is often that we work with low fluxes with noisy detectors [Herriot, 2000] and the dominant error is due to the noise. However, it is not optimal for the new generation of CCD with low readout noise and new laser guide star. For those cases, the noise is not limiting the WFS error and the QC is not optimum since we lose in precision.

Moreover, because of γ , the performances of the QC depend on the determination of the size of the spot as well as its shape. In presence of big motions of the spot on the CCD – for high atmospherical turbulence in open loop for example – , a saturation occurs [Hardy, 1998]. The error due to the saturation if the dominant ones at high flux (c.f. figure I.1.7).

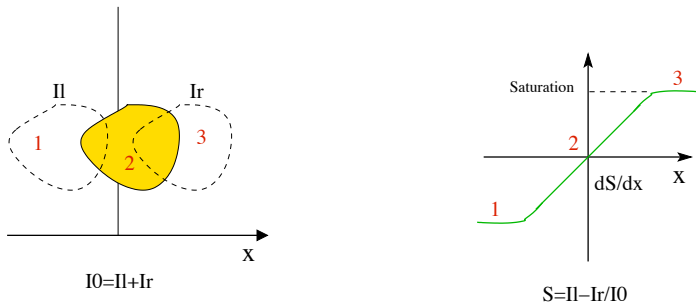


Figure I.1.7: Left: illustration of a spot on the QC. Right: Linearity curve that shows the saturation when the spot is displaced more than half its size. $S = (C_{mes})_x$

Calculation of γ for a Gaussian spot

The center of mass is $(C_{mes})_x = (I_l - I_r) / I_0$, where

$$I_l = \int_{-\infty}^{+\infty} \int_{-\infty}^0 I(x, y) dx dy = \int_{-\infty}^0 J(x) dx, \quad I_r = \int_{-\infty}^{+\infty} \int_0^{+\infty} I(x, y) dx dy = \int_0^{+\infty} J(x) dx, \quad (\text{I.1.19})$$

$$\text{where } J(x) = \int_{-\infty}^{+\infty} I(x, y) dy \quad (\text{I.1.20})$$

Since the spot is Gaussian,

$$I(x, y) = I(x)I(y) \text{ avec } I(x) = \frac{1}{\sqrt{2\pi\sigma^2}} e^{-x^2/2\sigma^2}, \quad I(y) = \frac{1}{\sqrt{2\pi\sigma^2}} e^{-y^2/2\sigma^2}.$$

To be sure the response is not biased, $\partial(C_{mes})_x/\partial x = 1$ (c.f. figure I.1.7). From the equations I.1.19, γ is equal to:

$$\gamma = \frac{I_0}{\partial I/\partial x - \partial I_r/\partial x} = \frac{1}{2 * J(0)} = \frac{\sqrt{\pi}\sigma}{\sqrt{2}} \quad (\text{I.1.21})$$

We will use this expression of γ as first approximation in the case of a spot distorted by the atmospheric turbulence. The difficulty will be to determine the value of σ .

Theoretical formula

For the QC, Eqs. I.1.11 become:

$$\sigma_{\Delta\phi, N_r}^2 = \kappa^2 4\pi^2 \frac{N_r^2}{N_{ph}^2} \text{ radians}^2 \text{ readout noise} \quad (\text{I.1.22})$$

$$\sigma_{\Delta\phi, N_{ph}}^2 = \kappa^2 \frac{\pi^2}{2} \frac{1}{N_{ph}} \text{ radians}^2 \text{ photon noise.} \quad (\text{I.1.23})$$

Pour une tache gaussienne, κ dépend de sa taille rms. Si l'on considère que la taille rms σ de la tache est donnée en radian (pour ce cas uniquement), on trouve que $\kappa = \gamma 2\pi/(\lambda/d) = \sqrt{2\pi} \sigma/(\lambda/d)$. Dans le cas d'une tache de diffraction, κ est égal à 1 [Rousset, 1999].

The weighted center of gravity (WCoG)

For the weighted center of gravity (WCoG) each pixel is associated to a different weight depending on its position on the CCD, thus its SNR. The contribution of the noisy pixels with low signal – like the one outside the spot – is attenuated. This method has been described and studied by [Nicolle et al., 2004]. The choice of the weighted function $P(x, y)$ is therefore important and depends on the SNR and the turbulence.

$$\hat{x}_{WCoG} = \frac{\sum x I(x, y) P(x, y)}{\sum I(x, y) P(x, y)}. \quad (\text{I.1.24})$$

The simplest case is when $P(x, y) = 1$ for $\sqrt{x^2 + y^2} < r$, which is the simple windowing. In the following I will use a Gaussian function with a FWHM N_w .

Nicolle et al. [2004] derived the theoretical formula of the phase error variance:

$$\sigma_{\Delta\phi, N_r}^2 = \alpha^{-1} \frac{\pi^3}{32(\ln 2)^2} \frac{N_r^2}{N_{ph}^2} \frac{(N_T^2 + N_w^2)^2}{N_{samp}^2} \text{ radians}^2, \text{ readout noise} \quad (\text{I.1.25})$$

$$\sigma_{\Delta\phi, N_{ph}}^2 = \alpha^{-1} \frac{\pi^2}{2\ln 2} \frac{1}{N_{ph}} \left(\frac{N_T}{N_{samp}} \right)^2 \frac{N_T^2 + N_w^2}{2 * N_T^2 + N_w^2} \text{ radians}^2, \text{ photon noise.} \quad (\text{I.1.26})$$

where α is the response coefficient. This coefficient has to be considered to have a non-biased measure of the position. It is possible to calculate this coefficient as well as the non-linearity coefficient, β following the same method as for the simple CoG:

$$(C_{meas})_x = \left(\frac{\sigma_W^2}{\sigma^2 + \sigma_W^2} \right) D_x - \sigma_{eq} \sqrt{\frac{2}{\pi}} \frac{e^{-C^2} - e^{-D^2}}{\Phi(D) + \Phi(C)} \quad (\text{I.1.27})$$

where σ_{eq} is defined as $\frac{1}{\sigma_{eq}^2} = \frac{1}{\sigma^2} + \frac{1}{\sigma_W^2}$, where σ_W^2 is the rms size of $P(x, y)$. Moreover, $C = \frac{W/2 - D_x}{\sigma_{eq}\sqrt{2}}$ et $D = \frac{W/2 + D_x}{\sigma_{eq}\sqrt{2}}$.

A first approximation gives

$$\alpha = \frac{\sigma_W^2}{\sigma^2 + \sigma_W^2} = \frac{N_W^2}{N_T^2 + N_W^2} \quad (\text{I.1.28})$$

In the following, I consider that all the measure are corrected from this response coefficient α . The validity domain is similar to the CoG one.

It is worth mention that like the windowing, we can consider a weighting function centered on the center of the FoV or centered on the pixel with the maximum intensity. In this report, I only considered the fixed weighting function.

I.1.3.2 The indirect methods: the correlation

This method is not new and has been studied in [Poyneer et al., 2003], [Michau et al., 1992], and [Noël, 1997]. The hardest part in the calculation of the correlation peak position.

Correlation calculation

The noisy image obtained at the focal plane of the lenslet array is correlated with the reference image. The reference function is an approximation of the image without any noise. This is therefore a Gaussian function with FWHM N_w . This appears to be optimal in presence of readout noise. If the photon noise dominate, the optimal reference function is the logarithmic of the Gaussian function. However, the difference was not significant enough to be worth the complication of computation in this study.

By definition, the correlation function $I_c(x, y)$ of $I(u, v)$ by the reference function $P(u, v)$ is:

$$I_c(x, y) = \sum_{u=-N_c/2}^{N_c/2} \sum_{v=-N_c/2}^{N_c/2} I(u, v)P(u + x, v + y), \quad (\text{I.1.29})$$

where N_c is the size of the matrix used in the calculation of the correlation. We need $N_c \geq 2N_{tot}$ to avoid truncation effect. It is simpler to calculate the correlation function in the Fourier domain since one property of the Fourier transform: the Fourier transform of a correlation of two functions is equal to the product of the Fourier transform of each function, one being conjugated.

$$I_c(x, y) = TF^{-1}[TF(I(x, y)) \times TF^*(P(x, y))], \quad (\text{I.1.30})$$

where $(x, y) \in [0 : 2N_{tot}, 0 : 2N_{tot}]$.

Using the Fourier transform, it is possible to over-sample the correlation function. The Fourier transform of each function is put in a matrix of size $2 * n \times N_{tot}$ before computing the inverse Fourier transform.

The choice of the reference FWHM is also a parameter. To optimize it, I introduced K_s such as $N_w = K_s N_{samp}$.

Using the correlation algorithm improves the contrast and reaches a better stability for lower SNR. However, the computation time might be a limitation for big telescopes. Moreover, it can be shown theoretically that the correlation should give us the best results in term of maximum-likelihood. For a point source, this advantage appear to be low. However, it will become important for extended sources.

All this looks appealing. However, there is a problem of peak determination. Indeed, there are different ways to proceed: one can use the thresholding or windowing, parabola fitting or Gaussian fitting.

Peak determination

Simple CoG The easiest way is here again to use the simple CoG defined earlier (Eq. I.1.10) with $N_c \times N_c$ the size of the matrix used for the correlation calculation and $(I_c)_{x,y}$ the value of the

correlation function at the pixel. This method is obviously not optimal for the same reason as the ones given above.

Windowing: as described earlier, we only consider a central part of the correlation function to calculate the CoG. Only a fixed window has been studied.

Thresholding: it gives an unbiased calculation of the correlation peak. When the SNR is low, it the threshold needs to be increased. Similarly to the direct thresholding of the image, we define T_{corr} as the percentage of the maximum such as the threshold be $T_{corr} * \max(I_c)$. The image used for the calculation of the CoG is defined as ($I_{res} = (I_c - T_{corr} * \max(I_{ini})) > 0$).

To be able to increase the threshold to get the optimal performances, we use the oversampling method described earlier. If the correlation function is not over-sampled, the thresholding level will be limited.

Parabola fitting This method has been described by Lisa Poyneer [Poyneer et al., 2003] and Vincent Michau. The goal is to fit the correlation function with a parabola, only close to the maximum.

If x_n is a number of points associated to a value I_n , and $n \geq 3$, we can define a parabola $f(x)$ such as $f(x) = a + bx + cx^2$. a, b and c are calculated to minimize:

$$\sum_{i=1}^n [I_i - f(x_i)]^2 = \sum_{i=1}^n [I_i - (a + bx_i + cx_i^2)]^2 \quad (\text{I.1.31})$$

Solving this system is equivalent to put the derivative by a, b , and c to zero, leading to:

$$\begin{cases} (E1) : \sum_{i=1}^n [I_i] = a \sum_{i=1}^n [1] + b \sum_{i=1}^n [x_i] + c \sum_{i=1}^n [x_i^2] \\ (E2) : \sum_{i=1}^n [x_i I_i] = a \sum_{i=1}^n [x_i] + b \sum_{i=1}^n [x_i^2] + c \sum_{i=1}^n [x_i^3] \\ (E3) : \sum_{i=1}^n [x_i^2 I_i] = a \sum_{i=1}^n [x_i^2] + b \sum_{i=1}^n [x_i^3] + c \sum_{i=1}^n [x_i^4] \end{cases}$$

Let's be x_0, I_0 the position and value of the maximum and x_i, I_i the position and value of the pixel i . Resolving the system $\{(E1),(E2),(E3)\}$ allows to find the parameters a, b et c and calculate the peak position, $X_c = x_0 - b/2c$.

Let's consider x_{-1}, x_0 et x_1 , then:

$$X_c = x_0 - 0.5 * \frac{I_1 - I_{-1}}{I_1 + I_{-1} - 2I_0}. \quad (\text{I.1.32})$$

This development has been done in one dimension (1D) and we are working with two dimensions images (2D). To use the formula, we first found the maximum (x_m, y_m) and then applied the equation I.1.33 to $(x_0 - 1, y_0), (x_0, y_0), (x_0 + 1, y_0)$ to find the peak in the X-coordinate and similarly for the Y-coordinates (c.f. Fig. I.1.8).

$$X_c = x_0 - 0.5 * \frac{I(x_1, y_0) - I(x_{-1}, y_0)}{I(x_1, y_0) + I(x_{-1}, y_0) - 2I(x_0, y_0)}. \quad (\text{I.1.33})$$

Gaussian fitting We used the function *Gaussfit* in IDL¹ to compute the fitting of the correlation function by a Gaussian. Here again we needed to work at 1D, and worked therefore on lines and

¹Interactive Data Language, software

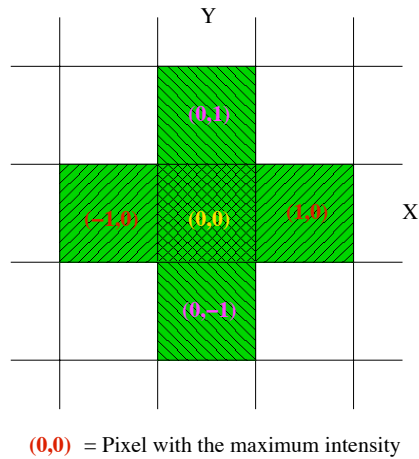


Figure I.1.8: Pixels used in the peak determination by the parabola fitting method.

columns separately.

For this method, we will first compare the 4 methods of peak correlation. The main result is that all methods are more or less equivalent except the windowing which introduces non-linearity.

Theoretical variance

Theoretical formula of the error variance have been developed with Vincent Michau in presence of readout noise [Michau, 2005] and for the thresholding method. Let's s be the threshold and D the domain for which $I_c(x, y) \geq s$, and D_c is the domain on which the function are defined. The correlation peak is then:

$$x_{corr} = \frac{\int_D x [I_c(x, y) - s] dx dy}{\int_D [I_c(x, y) - s] dx dy} = \frac{N_g}{D_g} \quad (\text{I.1.34})$$

We assume the reference function to be determinist and the denominator fluctuations negligible compared to the numerator ones. Then the error variance becomes:

$$\sigma_{x,corr}^2 = \frac{\langle N_g^2 \rangle - \langle N_g \rangle^2}{\langle D_g \rangle^2}, \quad (\text{I.1.35})$$

where

$$\langle N_g^2 \rangle - \langle N_g \rangle^2 = \int_D \int_D x x' \sigma_{I_c}^2(x, y, x', y') dx dy dx' dy', \quad (\text{I.1.36})$$

where $\sigma_{I_c}^2(x, y, x', y')$ is the variance of the correlation function. We can show that:

$$\begin{aligned} \sigma_{I_c}^2(x, y, x', y') = & \int_{D_c} \int_{D_c} P(u, v) P(u', v') [\langle I(u+x, v+y) I(u'+x', v'+y') \rangle \\ & - \langle I(u+x, v+y) \rangle \langle I(u'+x', v'+y') \rangle] du dv du' dv'. \end{aligned} \quad (\text{I.1.37})$$

But

$$\begin{aligned} & [\langle I(x, y) I(x', y') \rangle - \langle I(x, y) \rangle \langle I(x', y') \rangle] = \\ & \begin{cases} \sigma_b^2(x, y), & \text{if } (x, y) = (x', y') \\ 0, & \text{if } (x, y) \neq (x', y') \end{cases} \end{aligned} \quad (\text{I.1.38})$$

where $\sigma_b(x, y)$ is the noise density. In presence of readout noise, white noise, σ_b is constant and equal to N_r . Then

$$\sigma_C^2(x, y, x', y') = N_r^2 \int_{D_c} P(u, v) P(u + x - x', v' + y - y') du dv \quad (\text{I.1.39})$$

A development of Eq. I.1.35 gives:

$$\sigma_{N_r}^2 = N_r^2 \frac{\int_D \int_D x x' [C_{\langle P \rangle}(x - x', y - y')] dx dy dx' dy'}{\langle D_g \rangle^2}, \quad (\text{I.1.40})$$

where $C_{\langle P \rangle}$ is the autocorrelation of the function P . $\sigma_{N_r}^2$ is in pixels².

V. Michau developed a simplified expression of Eq. I.1.40 using that:

$$C_{\langle P \rangle}(x, y) \approx C_I(x, y)(D_c \otimes D_c)(x, y) \quad (\text{I.1.41})$$

close to the maximum. This function can be fitted by a parabola close to the maximum such as:

$$C_I(x, y) = N_{ph}^2 \left(1 - \frac{x^2 + y^2}{2\delta^2} \right) \quad (\text{I.1.42})$$

where δ is the FWHM of $C_{\langle P \rangle}$.

Therefore,

$$\sigma_{N_r}^2 = \frac{4\delta^2 N_r^2}{N_{ph}^2}. \quad (\text{I.1.43})$$

I.1.4 Program description

I.1.4.1 Shape of the spot

In this study I focussed on two types of sources:

- **A perfect flat wavefront** which gives a diffraction in the focal plane of the lenslet. As a first approximation, I consider the spot to be Gaussian. If D_x, D_y is the position of the center of gravity of the Gaussian then the intensity repartition on the detector is:

$$I(x, y) = \frac{N_{ph}}{2\pi\sigma^2} e^{-\frac{(x-D_x)^2 + (y-D_y)^2}{2\sigma^2}}, \text{ avec } N_{ph} = \int \int_{-\infty}^{+\infty} I(x, y) dx dy \quad (\text{I.1.44})$$

D_x and D_y are randomly defined using a Gaussian repartition of amplitude rms Dep_{amp} . In this report, I mainly chose $Dep_{amp} = 0.1$ pixel, equivalent to about 10% of the rms spot size for a Nyquist sampling. In some cases, the approximation of the diffraction spot by a Gaussian is not enough and it is needed to consider the *sinc*² function of the Airy disk:

$$I(x, y) = \text{sinc}^2\left(\frac{xd}{p\lambda}\right) \text{sinc}^2\left(\frac{yd}{p\lambda}\right), \quad (\text{I.1.45})$$

where $\text{sinc}(y) = \sin(\pi y)/(\pi y)$ and $p = (\lambda/d)/N_{samp}$.

- **Turbulent wavefront.** In AO, we will more likely have on the CCD a spot distorted by the turbulence than a diffraction spot. The spot distortion depends on the ratio d/r_0 : if $d/r_0 < 1$ the spot are close to be diffraction limited and the intensity can be described by Eq. I.1.45. If $d/r_0 > 3$, the spot maximum bursts into speckle.

To compute *phi*, I used the power spectrum of the phase, which is after propagation through all turbulent layers:

$$\Phi_{\varphi}(\mathbf{f}) = 0.0228 * (r_0)^{-5/3} * (f_{2D})^{-11/3}, \quad (\text{I.1.46})$$

for a Kolmogorov statistics. f is the two-dimensionnal spatial frequency. To get the phase from this expression, we se the inverse Fourier transform:

$$\varphi(x, y) = TF^{-1}[\sqrt{\Phi_{\varphi}(\mathbf{f}_{2D})} * [\text{random}(x) + i \text{random}(y)]], \quad (\text{I.1.47})$$

where $\text{random}(X)$ is the random function. Then the intensity repartition $I(x, y)$ is given by Fourier transform:

$$I(x, y) = N_{ph} |TF[Pup * (\cos(\phi) + i \sin(\phi))]|^2, \quad (\text{I.1.48})$$

where Pup is the pupil. In this case, the true centroid is the defined by the G-tilt:

$$D_x \propto \frac{1}{d^2} \int \int_{\text{sous-pupille}} \frac{\partial \phi}{\partial x} dx dy = \frac{1}{d} \int_0^d \phi(d, y) dy - \frac{1}{d} \int_0^d \phi(0, y) dy, \quad (\text{I.1.49})$$

I.1.4.2 Reliability of the result and robustness

If we do not set limits, the program always calculate an error variance. However, this variance might be wrong especially when the SNR is low. To be sure to trust our data, I introduced some validity tests in the program.

Test on the maximum intensity of the image. This condition is useful to verify that the image is not dominated by the noise and to be sure we are considering some signal. I set this condition at the beginning of the data processing to be $\max(I(x, y)) > 2 * N_r$.

Test on the error made. We assume that the measured center of mass can not be too far of the true value. Therefore, at each iteration we check that $(C_{mes})_{x/y} - D_{x/y}$ is less than $2 * \sigma$.

If one condition is not satisfied, the error for the iteration is set to zero and we increment a test variable Nul . If Nul reaches half of the iterations (500 in my program) the error variance is not considered and does not appear on the final graph.

Finally, a last test is made on the error variance itself. Again the error can not be too high and we set a higher limit for the variance equal to the rms size of the spot: $(\sigma_{err})^2 < \sigma^2$. In this study, the image is mainly Nyquist sampled, thus $(\sigma_{err})_{limite}^2 \approx 7 \text{ rad}^2$ (c.f. Eq. I.1.9).

I.1.4.3 Program architecture

The program has first been developed to verify the theoretical formulae in the simple case of a Gaussian spot. Then we used a spot distorted by the atmospherical turbulence. The architecture and the logic of the program is given on Fig. I.1.9.

Batch.pro Program that defines the parameters that I want to vary:

- Choice of the source: Gaussian, diffraction limited (*sinc*²) or limited by the turbulence
- N_{ph} : photon number per frame
- N_r : readout noise
- T et T_{corr} : % of the maximum to define the threshold value (on the direct image or the correlated function)
- N_w FWHM of the reference function

- K_s such as $N_w = K_s \sigma$
- n : over-sampling factor
- W : Window size

Main.pro This routine allocates the memory for the matrix and calls the following other routines:

PSF.pro Creation of the matrix with 1000 of PSF created by source.pro. We then add noise;

Source.pro PSF calculation depending on the choice of the source, without noise;

Centroid.pro Calculation of the CoG : calls the different routines depending on the choice of image processing;

Thres.pro Thresholding;

Win.pro Windowing and weighted CoG;

Corr.pro Correlation;

Quad.pro Quad Cell.

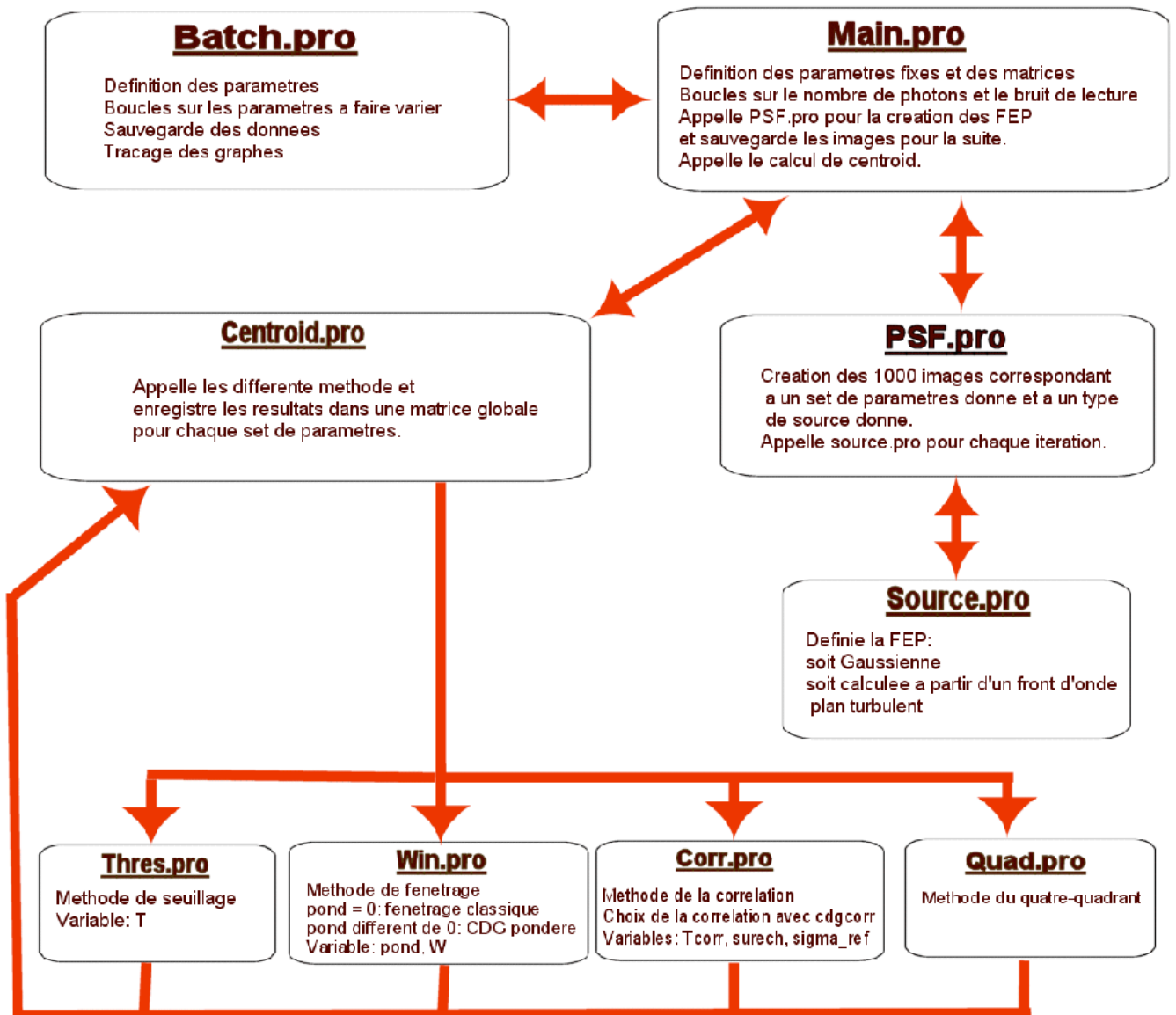


Figure I.1.9: Program architecture.

The number of iteration is 1000 per parameters. Also, unless stated, I considered well sampled images, $N_{samp} = 2$.

Table I.1.2 gives a summary of the methods and parameters studied as well as the figure related to it. The sign “-” means that the parameter does not exist for that box and the sign “?” means that I have not studied this set of method-parameter yet.

Table I.1.2: Summary

	Linearity	N_{samp}	spot	W_{fov} ou N_c	T_{ou} T_{corr}	N_w	n
CoG	Fig. 12	Fig. 11	Gaussian:	Fig. 16	-	-	-
	Fig. 13		Diffraction:	Fig. 15	-	-	-
	Fig. 14		Atmosphere:	Fig. 32, 33	-	-	-
Threshold	Fig. 17	-	Gaussian:	Fig. 16	Fig. 18, 19	-	-
			Diffraction:	-	?	-	-
			Atmosphere:	-	Fig. 34	-	-
WCoG	Eq.29	Fig. 11	Gaussian:	Fig. 21, 22	-	?	-
			Diffraction:	Fig. 21, 22	-	?	-
			Atmosphere:	Fig. 36, 37	-	Fig. 36	-
QC	Fig. 20		Gaussian:	-	-	-	-
			Diffraction:	-	-	-	-
			Atmosphere:	Fig. 35	-	-	-
Correlation windowing	Fig. 23		Gaussian:	Fig. 24	-	$= N_{samp}$	$= 1$
			Diffraction:	?	-	?	?
			Atmosphere:	?	-	?	?
Correlation threshold	Fig. 25	Fig. 10	Gaussian:	-	Fig. 26	Fig. 26	Fig. 27
			Diffraction:	-	?	?	?
			Atmosphere:	-	Fig. 40, 41	Fig. 39	$= 4$
Correlation parabola fitting			Gaussian:	-	-	N_{samp}	$= 2$
			Diffraction:	-	-	?	$= 2 ?$
			Atmosphere:	-	-	N_{samp}	$= 2$
Correlation Gaussian fitting	Fig. 28		Gaussian:	-	?	N_{samp}	$= 1$
			Diffraction:	-	?	?	$= 1?$
			Atmosphere:	-	?	N_{samp}	$= 1$

Table I.1.3 gives the summary of all the comparison done in between different methods.

Table I.1.3: Comparison of the results: Corr means comparison between different peak determination methods. All means comparison in between the different methods.

Gaussian	Corr	Fig. 29
Gaussian	All	Fig. 31
Atmosphere	Corr	Fig. 38
Atmosphere	All	Fig. 43, Fig. 44

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